

Deformáció jellemzése



\underline{r} : deformálatlan állapotban egy pont helye

$\underline{u}(\underline{r}, t)$ - elmozdulás v. r.

$$\underline{r} \rightarrow \underline{r} + \underline{u}(\underline{r})$$

$$\underline{r} + \Delta \underline{r} \rightarrow \underline{r} + \Delta \underline{r} + \underline{u}(\underline{r} + \Delta \underline{r})$$

$$\Delta \underline{r}' = \Delta \underline{r} + \underline{u}(\underline{r} + \Delta \underline{r}) - \underline{u}(\underline{r})$$

$$u_i(\underline{r} + \Delta \underline{r}) - u_i(\underline{r}) \approx \frac{\partial u_i}{\partial r_j} \Delta r_j$$

$$\Delta r'_i \approx \Delta r_i + \frac{\partial u_i}{\partial r_j} \Delta r_j = \left(\delta_{ij} + \frac{\partial u_i}{\partial r_j} \right) \Delta r_j$$

$$\beta_{ij} = \frac{\partial u_i}{\partial r_j} : \text{distorzó}$$

$$\hat{\beta} = \frac{\partial \underline{u}}{\partial \underline{r}}$$

Forgás: $\underline{v} = \underline{v}_0 + \underline{\omega} \times \underline{r}$

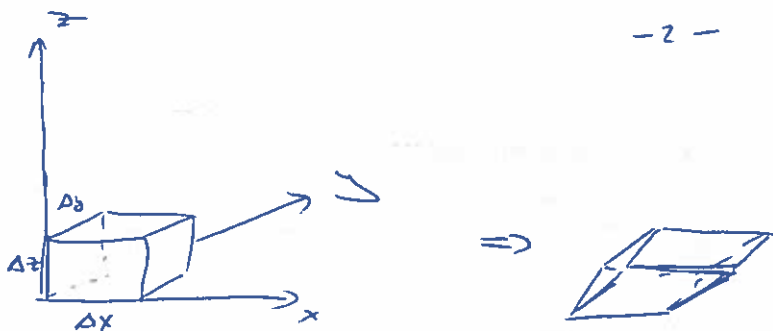
$$\epsilon_{ij} = \frac{1}{2} (\beta_{ij} + \beta_{ji}) = \frac{1}{2} \left(\frac{\partial u_i}{\partial r_j} + \frac{\partial u_j}{\partial r_i} \right)$$

$\hat{\epsilon}$ deformációs tenzor

$$\underline{u}(\underline{r}, t + \Delta t) - \underline{u}(\underline{r}, t) = \Delta \underline{\psi} \times \underline{r}$$

$$\Delta \left[\underline{u}(\underline{r} + \Delta \underline{r}) - \underline{u}(\underline{r}) \right] = \Delta \underline{\psi} \times \Delta \underline{r} = \Delta \hat{\beta} \Delta \underline{r}$$

\Downarrow
 either $\Delta \underline{\psi} \times \hat{\beta}$ or antisymmetric matrix



$$\Delta \underline{x}' = \left(1 + \frac{\partial u_1}{\partial r_1}, \frac{\partial u_2}{\partial r_1}, \frac{\partial u_3}{\partial r_1} \right) \Delta x$$

$$\Delta \underline{y}' = \left(\frac{\partial u_1}{\partial r_2}, 1 + \frac{\partial u_2}{\partial r_2}, \frac{\partial u_3}{\partial r_2} \right) \Delta y$$

$$\Delta \underline{z}' = \left(\frac{\partial u_1}{\partial r_3}, \frac{\partial u_2}{\partial r_3}, 1 + \frac{\partial u_3}{\partial r_3} \right) \Delta z$$

$$\Delta V' = \begin{vmatrix} 1 + \frac{\partial u_1}{\partial r_1} & \frac{\partial u_2}{\partial r_1} & \frac{\partial u_3}{\partial r_1} \\ \frac{\partial u_1}{\partial r_2} & 1 + \frac{\partial u_2}{\partial r_2} & \frac{\partial u_3}{\partial r_2} \\ \frac{\partial u_1}{\partial r_3} & \frac{\partial u_2}{\partial r_3} & 1 + \frac{\partial u_3}{\partial r_3} \end{vmatrix} \Delta x \Delta y \Delta z \approx \left(1 + \frac{\partial u_1}{\partial r_1} \right) \left(1 + \frac{\partial u_2}{\partial r_2} \right) \left(1 + \frac{\partial u_3}{\partial r_3} \right) \Delta x \Delta y \Delta z$$

$$\approx \left[1 + \left(\frac{\partial u_1}{\partial r_1} + \frac{\partial u_2}{\partial r_2} + \frac{\partial u_3}{\partial r_3} \right) \right] \Delta x \Delta y \Delta z = (1 + \text{sp} \hat{e}) \Delta V$$

Dinamika



$$\Delta \underline{F}_k = \int_V(\underline{r}) dV$$

$$\Delta \underline{F}_f \sim \Delta \underline{A}$$

$$\Delta \underline{F}_f = \hat{G}(\underline{r}) \Delta \underline{A}$$

$$\underline{F}_k = \int_V \underline{f}(\underline{r}) dV$$

$$\underline{F}_f = \oint_F \hat{G}(\underline{r}) d\underline{A}$$

$$\underline{F} = \int_V \underline{f}(\underline{r}) dV + \oint_{\partial V} \hat{G}(\underline{r}) d\underline{A}$$

A del. integrál 1. komponense: $\oint \sigma_{11} dx + \sigma_{12} dy + \sigma_{13} dz = \int \left(\frac{\partial \sigma_{11}}{\partial x_1} + \frac{\partial \sigma_{12}}{\partial x_2} + \frac{\partial \sigma_{13}}{\partial x_3} \right) dV$

↑
 $\frac{\partial \sigma_{1j}}{\partial x_j}$

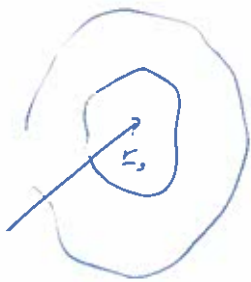
$$\oint \hat{G} dA = \int \text{div } \hat{G} dV$$

$$\left(\int \text{div } \hat{G} dV \right)_i = \int \frac{\partial \sigma_{1j}}{\partial x_j} dV$$

⇒

$$\underline{F} = \int_V \left[f(x) + \text{div } \hat{G} \right] dV = 0$$

= 0 *eigenfüßbar*



$$\begin{aligned} \underline{F}_k &= \int f \, dV + \oint \hat{\underline{G}} \, dA = \\ &= \int (f + \text{div } \hat{\underline{G}}) \, dV \end{aligned}$$

$$\Delta F = \hat{\underline{G}} \Delta A$$

$$f + \text{div } \hat{\underline{G}} = 0 \quad \text{egyenlet}$$

$$M \underline{\ddot{r}}_0 = \underline{F}_k$$

$$M \underline{\ddot{r}}_0 = \sum_{i=1}^N m_i \underline{\ddot{r}}_i = \frac{d}{dt} \left[\sum_{i=1}^N m_i \underline{v}_i \right]$$

$$M \underline{\ddot{r}}_0 = \frac{d}{dt} \left[\int \underline{\dot{u}} S(\underline{r}) \, dV \right] \approx \int \underline{\ddot{u}} S \, dV$$

↳ kicsik a deformációk

$$\boxed{S \underline{\ddot{u}} = f + \text{div } \hat{\underline{G}}}$$

$$\underline{F}(\underline{r}, \underline{v}, t)$$

↓

$\hat{\underline{G}}(\underline{\hat{\epsilon}}, \underline{\dot{\hat{\epsilon}}}, t) \leftarrow$ Anyagra jellemző, meg kell adni...

$$\underline{\sigma}_{ij} = \underline{\sigma}_{ji} \Rightarrow \text{A forgatónyomaték 0.}$$

↳ Teljesen = pontszerű impulzusmomentumra vonatkozó tétel.

↳ pl. betonban lephetnek fel forgatónyomatékok: Cosserat - testek...

~~$\underline{\sigma}_{ij} = C_{ijkl} \epsilon_{kl}$~~

$$\underline{\sigma}_{ij} = C_{ijkl} \epsilon_{kl}$$

Általánosított Hooke-törvény

$$\hat{\underline{\sigma}} = \hat{\underline{C}} : \hat{\underline{\epsilon}}$$

pl. az a ből változik, de

~~$E_{ij} = E_{ji}$~~

$C_{ijkl} = C_{jilk}$, mert $G_{ij} = G_{ji}$

$C_{ijkl} = C_{ijlk}$, mert $\epsilon_{ij} = \epsilon_{ji}$, mert ugyanazok

↓

36 főtlen váltás

↳ Rugalmas test energidaja



$\sigma = E \epsilon$

$\frac{F}{A} = E \frac{\Delta l}{l}$ $F = \cancel{EA} \frac{EA}{l} \Delta l = D \Delta l$

$W = \frac{D}{2} \Delta l^2 = \frac{1}{2} \frac{EA}{l} \Delta l^2 = \frac{1}{2} E A l \left(\frac{\Delta l}{l}\right)^2$

$W = \frac{W}{V} = \frac{1}{2} E \epsilon^2 = \frac{1}{2} G \epsilon$

A'ltalános esetben:

$w = \frac{1}{2} \epsilon_{ij} C_{ijkl} \epsilon_{kl}$

- Azd. Aerebrium, hogy az osszes tulajdonasj az energis'bol parmozthato legyen.

⇔

$C_{ijkl} = C_{klij}$

↳ 21 főtlen váltás

$$\left. \sigma_{mn} = \frac{dw}{d\varepsilon_{mn}} \right| = \frac{d}{d\varepsilon_{mn}} \sum_{ijkl} \frac{1}{2} \varepsilon_{ij} C_{jilk} \varepsilon_{kl} = C_{mnji} \varepsilon_{ij}$$

↳ ez is lehetne a $\hat{\sigma}$ definíciója

21 gyűlés nélkül \Rightarrow a kristály szimmetriája tudja ezt csökkenteni.

Isotrop anyagok

Pl. polikristályos anyagok, műanyag

$\mathbb{3}$ $Sp \hat{\varepsilon} \quad Sp(\hat{\varepsilon} \cdot \hat{\varepsilon}) \quad Sp(\hat{\varepsilon} \cdot \hat{\varepsilon} \cdot \hat{\varepsilon})$ ← ez harmadrendű, ezért

↳ csak minden koordinátarendszerben meggyezzenek $w = \varepsilon_{ij} C_{jilk} \varepsilon_{kl}$ típusú ε_{kl} függvények lehetnek

$$w = \frac{\lambda}{2} (Sp \hat{\varepsilon})^2 + \mu Sp(\hat{\varepsilon} \cdot \hat{\varepsilon}) = \mu \varepsilon_{ij} \varepsilon_{ij} + \frac{\lambda}{2} (\varepsilon_{kk})^2$$

μ, λ : Lamé-állandók.

$$\sigma_{mn} = \frac{dw}{d\varepsilon_{mn}} = 2\mu \varepsilon_{mn} + \lambda \varepsilon_{kk} \cdot \delta_{mn}$$

$$\varepsilon_{ij} = \frac{1}{2\mu} \sigma_{ij} + \frac{\lambda}{2(\lambda + \mu)} \delta_{ij} \varepsilon_{kk} = \frac{1}{2\mu} \left(\sigma_{ij} - \frac{1}{3} \delta_{ij} \varepsilon_{kk} \right) + \left(\frac{2\mu}{3} + \lambda \right) \delta_{ij} \varepsilon_{kk}$$

modulusok
 a fog van
 tehát nyírás esetén csak ez

K: kompressziómodulus

Ha csak isotrop összenyomás van akkor csak ez számít.

Mi az $\epsilon(\sigma)$ összefüggés?

$$\sigma_{ee} = 2\mu \epsilon_{ee} + 3\lambda \epsilon_{ee} \quad \rightarrow \quad \epsilon_{ee} = \frac{1}{2\mu + 3\lambda} \sigma_{ee}$$

$$\sigma_{ij} = 2\mu \epsilon_{ij} + \frac{\lambda}{2\mu + 3\lambda} \delta_{ij} \sigma_{ee}$$

$$\epsilon_{ij} = \frac{1}{2\mu} \left[\sigma_{ij} - \frac{\lambda}{2\mu + 3\lambda} \delta_{ij} \sigma_{ee} \right]$$

Egységnyi σ_{ij} kés:

$$\sigma = \begin{pmatrix} \sigma & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$$\epsilon = \begin{pmatrix} \frac{1}{2\mu} \left(1 - \frac{\lambda}{2\mu + 3\lambda}\right) \sigma & 0 & 0 \\ 0 & -\frac{1}{2\mu} \frac{\lambda}{2\mu + 3\lambda} \sigma & 0 \\ 0 & 0 & -\frac{1}{2\mu} \frac{\lambda}{2\mu + 3\lambda} \sigma \end{pmatrix}$$

$$\frac{1}{E} = \frac{1}{2\mu} \left(1 - \frac{\lambda}{2\mu + 3\lambda}\right) = \frac{1}{2\mu} \left(\frac{2\mu + 3\lambda - \lambda}{2\mu + 3\lambda}\right) = \frac{1}{\mu} \frac{\mu + \lambda}{2\mu + 3\lambda} \quad \leftarrow \text{nem lehet negatív}$$

$$\nu = - \frac{\epsilon_{22}}{\epsilon_{11}}$$

L teljességgel $\nu < 0,5$ kelt kelt.

Ismetlis

Deformáció

$u(x, y, z)$

↓

$\hat{\rho}(x, y, z) = \underline{\nabla} u = \frac{\partial u}{\partial \underline{r}} \quad ; \quad \hat{\rho}_{ij} = \frac{\partial u_i}{\partial r_j} = \partial_j u_i$

↓

$\hat{\epsilon} = \text{sym} \hat{\rho} = \frac{1}{2} (\hat{\rho} + \hat{\rho}^T) \quad \epsilon_{ij} = \frac{1}{2} (\rho_{ij} + \rho_{ji}) = \frac{1}{2} (\partial_j u_i + \partial_i u_j)$

Állomány

$\Delta E = \hat{\sigma} \Delta A$

$\hat{\sigma} = \hat{C} \hat{\epsilon} \quad ; \quad \sigma_{ij} = C_{ijkl} \epsilon_{kl}$

Isotropia

$\sigma_{ij} = 2\mu \epsilon_{ij} + \lambda \delta_{ij} \epsilon_{kk} = 2\mu \delta_{ie} \delta_{jk} \epsilon_{ek} + \lambda \delta_{ij} \delta_{ke} \epsilon_{ek}$

$\hookrightarrow C_{ijkl} = 2\mu \delta_{ie} \delta_{jk} + \lambda \delta_{ij} \delta_{ke}$

$\epsilon_{ij} = \frac{1}{2\mu} \left[\sigma_{ij} - \frac{\lambda}{2\mu + 3\lambda} \delta_{ij} \sigma_{kk} \right]$

mozgásegyenlet

$\rho \ddot{u}_i = f_i + \text{div} \hat{\sigma} \quad ; \quad \rho \ddot{u}_i = f_i + \frac{\partial}{\partial r_j} \sigma_{ij} = f_i + \partial_j \sigma_{ij}$

~~Egyenlet~~

~~Állomány~~

Isotropia mozgásegyenlet: $\rho \ddot{u}_i - f_i = \partial_j \sigma_{ij} = \partial_j (2\mu \epsilon_{ij} + \lambda \delta_{ij} \epsilon_{kk}) = \partial_j \left(2\mu \frac{1}{2} (\partial_i u_j + \partial_j u_i) + \lambda \delta_{ij} (\partial_k u_k) \right)$
 $= \mu \partial_j^2 u_i + \mu \partial_i \partial_j u_j + \lambda \delta_{ij} \partial_j \partial_k u_k = \mu \partial_j^2 u_i + (\lambda + \mu) \partial_i \partial_j u_j$

$\rho \ddot{u}_i - f_i = \mu \partial_j^2 u_i + (\lambda + \mu) \partial_i \partial_j u_j \quad ; \quad \rho \ddot{u}_i - f_i = \mu \text{div grad } u + (\lambda + \mu) \text{grad div } u$

Isotropia mozgásegyenlet. \triangle

Eigenrészben:

$$-f_i = \mu \frac{\partial^2 u_i}{\partial x_j^2} + (\lambda + \mu) \frac{\partial^2 u_j}{\partial x_i^2} ; \quad -f = \mu \Delta u + (\lambda + \mu) \text{grad div } u$$

$$\Delta \phi = -\frac{1}{\epsilon_0} \rho$$

Saját sűrű alett megajtsa' rind esete

$$\underline{u}(x, y, z) \approx \begin{pmatrix} u_x(x, y, z) \\ u_y(x, y, z) \\ \vdots \\ u_z(z) \end{pmatrix} \Rightarrow \hat{\epsilon}(x, y, z) = \begin{pmatrix} \partial_x u_x & \frac{1}{2}(\partial_x u_y + \partial_y u_x) & \frac{1}{2} \partial_x u_z \\ \frac{1}{2}(\partial_x u_y + \partial_y u_x) & \partial_y u_y & \frac{1}{2} \partial_y u_z \\ \vdots & \vdots & \vdots \\ \frac{1}{2} \partial_x u_z & \frac{1}{2} \partial_y u_z & \partial_z u_z \end{pmatrix}$$

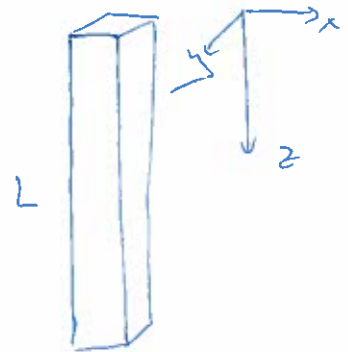
A benn hely mint az egykijelji nyújtással: $\hat{G} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & G(z) \end{pmatrix}$

Pr. Innen:

$$\epsilon_{ij} = \frac{1}{2\mu} \left[G_{ij} - \frac{2}{2\mu + 3\lambda} G_{ij} \sigma_{kk} \right] = \frac{1}{2\mu} \left[G_{ij} - \frac{2}{2\mu + 3\lambda} G_{ij} \sigma_{kk} \right]$$

$$\hat{\epsilon} = \begin{pmatrix} \frac{1}{2\mu} \frac{2}{2\mu + 3\lambda} G(z) & 0 & 0 \\ 0 & -\frac{1}{2\mu} \frac{2}{2\mu + 3\lambda} G(z) & 0 \\ 0 & 0 & \frac{1}{2\mu} \left(1 - \frac{2}{2\mu + 3\lambda} \right) G(z) \end{pmatrix}$$

$\frac{1}{E}$



$$\hookrightarrow \partial_z u_z = u_z'(z) = \frac{1}{E} G(z)$$

$$-f = \text{div } \hat{G} = \partial_z G(z) = G'(z) \begin{pmatrix} 0 \\ 0 \\ \partial_z G(z) \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ G'(z) \end{pmatrix}$$

$$\begin{pmatrix} 0 \\ 0 \\ -S_g \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ G'(z) \end{pmatrix} \Rightarrow -S_g = G'(z) = E \cdot u_z''(z)$$

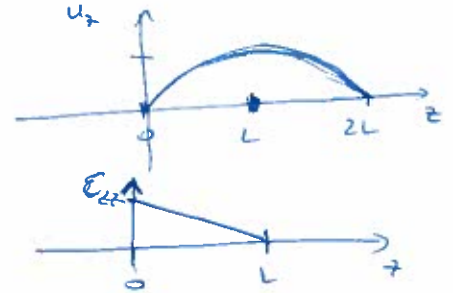
$$u_z(z) = A + Bz - \frac{\rho g}{2E} z^2$$

Határ-feltételek:

$$\begin{cases} u_z(0) = 0 \Rightarrow A = 0 \\ \sigma(L) = 0 \Rightarrow B - \frac{\rho g}{E} L = 0 \Rightarrow B = \frac{\rho g}{E} L \end{cases}$$

$$B - \frac{\rho g}{E} L = 0 \Rightarrow B = \frac{\rho g}{E} L$$

$$u_z(z) = \frac{\rho g}{E} (Lz - \frac{z^2}{2}) = -\frac{\rho g}{2E} z(z-2L)$$



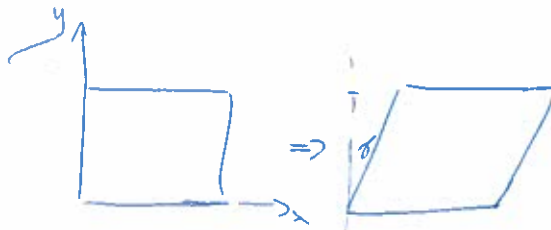
$$\epsilon_{zz}(z) = u_z'(z) = \frac{\rho g}{E} (L - z)$$

$$\sigma(z) = E \epsilon_{zz}(z) = \rho g (L - z) \Rightarrow \sigma(0) = \rho g L$$

$$L' = L + u(L) = L + \frac{\rho g}{2E} \cdot L^2 \quad F = \sigma(0) \cdot A = \rho g A L = mg$$

Csavarás

→ Uptitási deformáció



$$u_x(y) = y \cdot \gamma \approx \gamma \cdot y$$

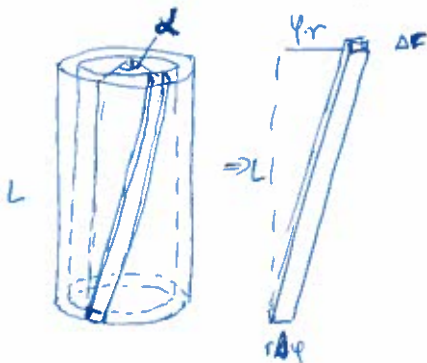
$$\underline{u}(x, y, z) = \begin{pmatrix} u_x(y) \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} y \cdot \gamma \\ 0 \\ 0 \end{pmatrix}$$

$$\Rightarrow \underline{\epsilon} = \begin{pmatrix} 0 & \frac{1}{2}\gamma & 0 \\ \frac{1}{2}\gamma & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$$\sigma_{ij} = 2\mu \epsilon_{ij} + \lambda \sum_j \epsilon_{jj} E_{ii}$$

$$\underline{\sigma} = \begin{pmatrix} 0 & \mu\gamma & 0 \\ \mu\gamma & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$$\Rightarrow \tau = \mu\gamma, \quad \gamma = \frac{\tau}{\mu}$$

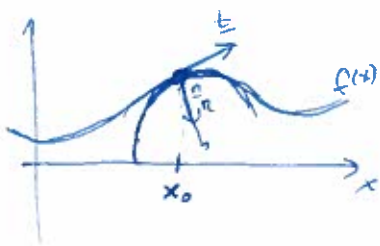


$$\Rightarrow \gamma = \frac{dr}{L} \rightarrow \tau = \mu\gamma = \mu \frac{r}{L} \cdot d\alpha \Rightarrow \Delta F = \tau \cdot \Delta A = \mu \frac{r}{L} d\alpha \cdot r \Delta\varphi \Delta r$$

$$\Delta \Pi = \Delta F \cdot r = \frac{\mu}{L} \cdot r^3 \cdot d\alpha \Delta\varphi \Delta r$$

$$\Pi = \int_0^{2\pi} \int_0^R \frac{\mu}{L} \cdot r^3 \cdot d\varphi \Delta r = 2\pi \frac{\mu}{L} \cdot \frac{R^4}{4} = \frac{\pi}{2} \cdot \frac{R^4}{L} \cdot \frac{d\alpha}{1}$$

Parabola sugar



$$\begin{cases} x(t) = t \\ y(t) = f(t) \end{cases}$$

$$v(t) = 1$$

$$a_x(t) = 0$$

$$v_y(t) = f'(t)$$

$$a_y(t) = f''(t)$$

$$v(t) = \sqrt{1 + f'(t)^2}$$

$$\underline{t} = \frac{v}{v} = \frac{1}{\sqrt{1 + f'(t)^2}} \begin{pmatrix} 1 \\ f'(t) \end{pmatrix}$$

$$\underline{a} = \dot{v} \underline{t} + \frac{v^2}{R} \underline{n} \quad / \cdot \underline{n}$$

$$|\underline{a} \cdot \underline{n}| = \frac{v^2}{R}$$

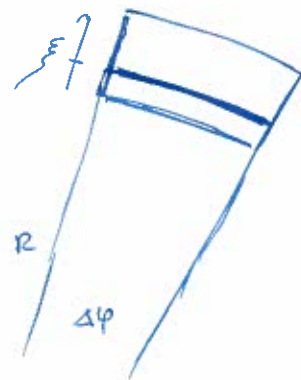
$$\underline{n} = \frac{1}{\sqrt{1 + f'(t)^2}} \begin{pmatrix} -f'(t) \\ 1 \end{pmatrix}$$

$$\underline{a} \cdot \underline{n} = \frac{1}{\sqrt{1 + f'(t)^2}} f''(t)$$

$$\Rightarrow \frac{v^2}{R} = \frac{1}{\sqrt{1 + f'(t)^2}} \cdot |f''(t)|$$

$$\Rightarrow \boxed{\frac{1}{R} = \frac{|f''(t)|}{(1 + f'(t)^2)^{3/2}}}$$

Lehajlás



$$\epsilon_{xx}(\xi) = \frac{(R + \xi) \Delta\varphi - R \Delta\varphi}{R \Delta\varphi} = \frac{\xi}{R} = -\xi h''(x) \xi$$

$$\sigma_{xx}(\xi) = E \cdot \epsilon_{xx}(\xi) = -E \cdot \xi h''(x) \xi$$

A lehajlás része: $F_c = 0, M = 0$

↓
 neutralis vonal meghatározása

Inertál kör. dra

M=0:



$$M = \int_R \sigma_{xx}(\xi) \cdot \xi \, d\xi \, d\varphi - F(L-x) = -E \cdot h''(x) \xi \int \xi^2 \, d\xi \, d\varphi - F(L-x) =$$

$$= -E \cdot I \cdot h''(x) - F(L-x) = 0$$

I ← másodrendű fluktuáció

$$h''(x) \xi = \frac{F(L-x)}{EI} \Rightarrow h''(x) = \frac{F}{EI} (x-L)$$

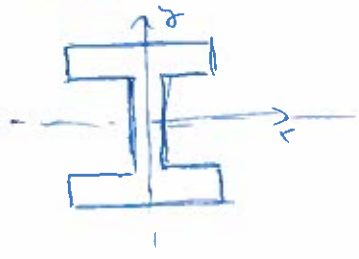
$$z''(x) = \frac{F}{EI} (x-L) \Rightarrow z'(x) = \frac{F}{EI} \left(\frac{x^2}{2} - Lx \right) \Rightarrow +B \Rightarrow z(x) = \frac{F}{EI} \left(\frac{x^3}{6} - L \frac{x^2}{2} \right) + Bx + A$$

Határfeltételek: $\begin{cases} z(0) = 0 \Rightarrow A = 0 \\ z'(0) = 0 \Rightarrow B = 0 \end{cases}$

$$z(x) = \frac{F}{EI} \left(\frac{x^3}{6} - L \frac{x^2}{2} \right)$$

A behajlás: $s = |z(L)| = \left| \frac{F}{EI} \left(\frac{L^3}{6} - L \frac{L^2}{2} \right) \right| = \frac{F}{EI} \cdot \frac{L^3}{3}$

A másodrendű felületi geometria:

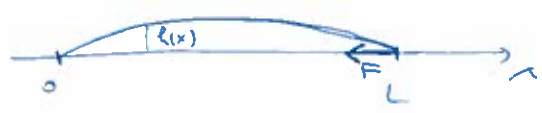


$$I = \int y^2 dx dy$$

tegyünk: $\int_{-\frac{a}{2}}^{\frac{a}{2}} dx \int_{-\frac{b}{2}}^{\frac{b}{2}} dy y^2 = a \left[\frac{y^3}{3} \right]_{-\frac{b}{2}}^{\frac{b}{2}} = \frac{ab^3}{12}$

Behajlás: $s = \frac{1}{EI} \cdot \frac{F}{2} \cdot \frac{1}{3} \left(\frac{L}{2} \right)^3 = \frac{F}{EI} \cdot \frac{L^3}{48}$

Kritérius



$$M = Fz(x) + EI \cdot z''(x) = 0$$

$$z''(x) + \frac{F}{EI} z(x) = 0$$

Megoldás: $z(x) = 0$

$$z(x) = A \cdot \sin(kx + x_0), \quad k = \sqrt{\frac{F}{EI}}$$

Határfeltételek: $\begin{cases} z(0) = 0 \Rightarrow x_0 = 0 \\ z(L) = 0 \Rightarrow k \cdot L = n\pi \end{cases}$

$n=0: z(x) = 0$

$n=1: k = \frac{\pi}{L} = \sqrt{\frac{F}{EI}} \Rightarrow \left[F = EI \cdot \frac{\pi^2}{L^2} = F_1 \right]$ Euler-cső

$n=2: k = 2 \frac{\pi}{L} = \sqrt{\frac{F}{EI}} \Rightarrow F = 4 EI \frac{\pi^2}{L^2} = 4 F_1$

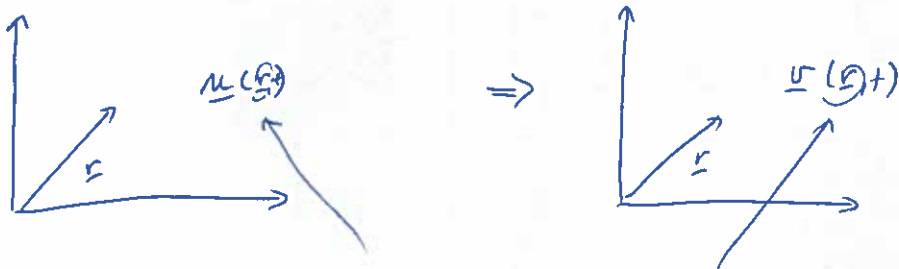
Foly = de'kok

$$\underline{\mathbb{F}} = (\underline{r}, \dot{\underline{r}}, t) \Rightarrow \hat{\mathbb{G}}(\hat{\underline{c}}, \hat{\underline{c}}, t)$$

csak $\hat{\underline{c}}$: pillanatpont

csak $\hat{\underline{c}}$: f. f. de'k

mindkettő: vektorok, \mathcal{G} l. kötés



A két \underline{r} nem ugyanaz
referenciadlugó \leftrightarrow megfigelési pont

Altíráz formálkötök: ~~v(r, t)~~

$$\frac{\partial \underline{u}(\underline{r}, t)}{\partial t} = \underline{v}(\underline{r} + \underline{u}(\underline{r}, t), t)$$

f. f. de'k: $S(\underline{r}, t) \approx \text{áll}$

g. g. $S(\underline{r}, t)$ nem állandó.

$$\rho(r,t), \underline{v}(r,t), \hat{G}(r,t)$$

↳ ρ et \underline{v} nem független



$$\rho \underline{v} \cdot \underline{n} \cdot \Delta t \cdot \Delta A$$

$$\begin{aligned} \Delta m &= - \oint \rho \underline{v} \cdot \underline{n} dA \Delta t = - \oint \rho \underline{v} \cdot d\underline{A} \cdot \Delta t = \\ &= \left(\frac{d}{dt} \int \rho dV \right) \Delta t \end{aligned}$$

$$\frac{d}{dt} \int \rho dV = - \oint \rho \underline{v} \cdot d\underline{A}$$

$$\int \frac{\partial \rho}{\partial t} dV = - \int \text{div}(\rho \underline{v}) dV$$

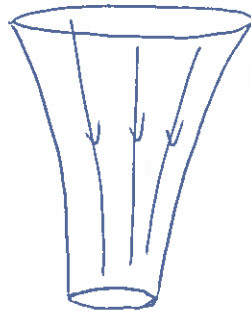
$$\boxed{\frac{\partial \rho}{\partial t} + \text{div}(\rho \underline{v}) = 0}$$

Kontinuitási egyenlet

Ha $\rho = \text{állandó} \Rightarrow \text{div} \underline{v} = 0$

Stacionárius áramlás

$$\underline{v}(r), \rho(r)$$



$$\oint \rho \underline{v} \cdot d\underline{A} = 0$$

$$\rho_1 v_1 A_1 = \rho_2 v_2 A_2$$

$$\hat{\sigma}(\dots) = ?$$

$$\Delta \underline{F} \sim \Delta \underline{A} \Rightarrow \Delta \underline{F} = -P \Delta \underline{A} \Rightarrow \hat{\sigma} = \begin{pmatrix} -P_{11} & 0 & 0 \\ 0 & -P_{11} & 0 \\ 0 & 0 & -P_{11} \end{pmatrix}$$

↑ Pascal-törvény

$$0 = \text{div } \hat{\sigma} + \underline{f}$$

$$(\text{div } \hat{\sigma})_x = -\frac{\partial P}{\partial x} \Rightarrow \text{div } \hat{\sigma} = -\text{grad } P$$

$$-\text{grad } P + \underline{f} = 0$$

grav. potenciál

gravitációs vektor: $\underline{f} = \rho \underline{g} = -\rho \cdot \text{grad } \phi$

$$\boxed{\text{grad } P + \rho \cdot \text{grad } \phi = 0}$$

ρ függést a s-től: $\rho V = \frac{m}{n} R T \Rightarrow \frac{P}{\rho} = \frac{R}{n} T$

ρ = all. összenyomhatatlan folyadék.

$$\Rightarrow \text{grad}(P + \rho \phi) = 0$$

$$P + \rho \phi = c = \text{all.}$$

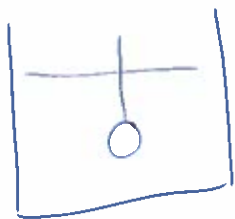
↳ azonos zömésű és ekvipotenciális felületek megegyeznek.

Főlk. felület:

$$P - \rho g h = P_0$$

$$P = P_0 + \rho g h$$

Felhajtás



$$\underline{F} = \oint \hat{G} d\underline{A}$$

Eggenisfban: $\text{div } \hat{G} + \underline{f} = 0$

Tfh viz van a test felett: $\underline{F} = \oint \hat{G} d\underline{A} = \int \text{div } \hat{G} dV = - \int \underline{f} dV =$
 $= - \rho g V$

barometrikus magasságformula

$$-\text{grad } p + \rho \underline{g} = 0$$

$$-\frac{dp}{dz} + \rho g = 0$$

$\left(\frac{p}{\rho} = \frac{R}{M} T = \text{const} \Rightarrow \rho = \frac{p}{\frac{R}{M} \cdot T} \right)$

$$\frac{dp}{dz} = - \frac{\rho}{\frac{R}{M} \cdot T} \cdot p$$

$$p(z) = p_0 \cdot e^{-\frac{g \cdot z}{\frac{R}{M} T}}$$

$$\Rightarrow \rho(z) = \rho_0 \cdot e^{-\frac{\rho_0 g \cdot z}{\frac{R}{M} T}} = \rho_0 e^{-\frac{mgz}{kT}} = \rho_0 e^{-\frac{E_p}{kT}}$$

Barometrikus magasságformula - kísérlet

Forgó fűzők felzése

← összemeghatlan fűzők

$-grad P + f = 0 \quad f = -\rho grad \phi$

forgó koordináta rendszerben:

$f = \rho \cdot g + \rho \omega^2 \cdot \underline{s} = -\rho grad (gz + \frac{\omega^2}{2}(x^2 + y^2))$



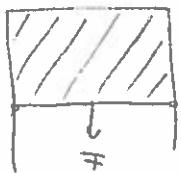
$grad (-\rho gz + \rho \frac{\omega^2}{2}(x^2 + y^2) - P) = 0$

$\hookrightarrow -\rho gz + \rho \frac{\omega^2}{2}(x^2 + y^2) - P = -P_0 \quad \leftarrow \text{bárhol}$

$\left| \rho gz = \rho \frac{\omega^2}{2}(x^2 + y^2) \right| \quad \leftarrow \text{o felületen } (P = P_0)$

→ forgó paraboloid

Felület feszültség (kísérlet)

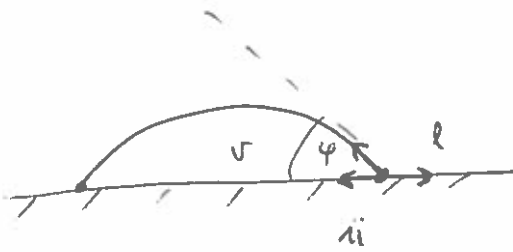


$F = 2 \alpha \cdot l$

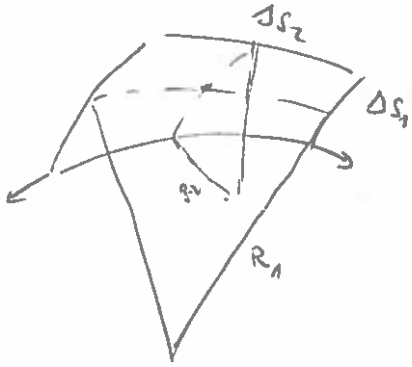
← 2 oldal van a felületnek

$\Delta W = F \cdot \Delta x = \alpha \cdot 2 l \cdot \Delta x = \alpha \cdot \Delta A$

$\Delta W = \alpha \cdot \Delta A$



$$\cos \varphi = \frac{\Delta u_l - \Delta u_r}{\Delta r l}$$



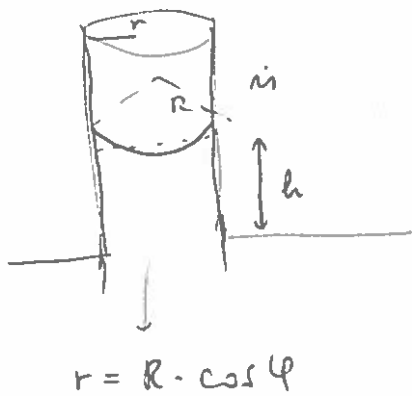
$$\Delta F = \alpha \Delta S_1$$

$$\Delta F_f = 2 \cdot \alpha \cdot \Delta S_1 \cdot \cos \varphi = \beta \alpha \Delta S_1 \frac{\Delta S_2}{2R_1}$$

$$\Delta F_f = \alpha \left(\frac{1}{R_1} + \frac{1}{R_2} \right) \Delta S_1 \Delta S_2$$

$$P = \alpha \left(\frac{1}{R_1} + \frac{1}{R_2} \right) \quad (\text{luft. fehlig})$$

Uegen Uen bis



$$E(h) = \rho \cdot r^2 \pi \cdot h \cdot g \frac{h}{2} - \alpha_{lu} 2\pi r h + \alpha_{lu} 2\pi r l$$

$$\frac{dE}{dh} = \rho r^2 \pi \cdot g h + (\alpha_{lu} - \alpha_{lu}) 2\pi r = 0$$

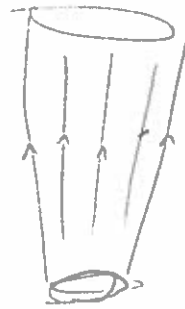
$$h = \frac{2(\alpha_{lu} - \alpha_{lu})}{\rho \cdot r \cdot g} = \frac{2}{\rho r g} \alpha_{lu} \cdot \cos \varphi =$$

$$= \frac{2 \alpha_{lu}}{\rho g R}$$

Analysis

→ Physikale Beschreibung

$v(x,t), S(x,t), p(x,t)$

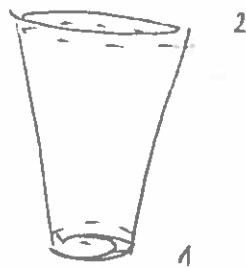


$\rho v A = c$

$\frac{\partial \rho}{\partial t} + \text{div}(\rho v) = 0$

$\hat{\sigma} = \begin{pmatrix} -p & 0 & 0 \\ 0 & \tau & 0 \\ 0 & 0 & -p \end{pmatrix} \rightarrow$ keil's fjdik

Energiesymmetrie:



$\frac{1}{2} \Delta m v_2^2 - \frac{1}{2} \Delta m v_1^2 = p_1 A_1 v_1 \Delta t - p_2 A_2 v_2 \Delta t + \Delta m U_1 - \Delta m U_2 + \Delta(\Delta W_b)$

→ Ordnung der Stellen

fjdikura = 0, net

ad kegsterenik
vanna

$\frac{1}{2} v_2^2 - \frac{1}{2} v_1^2 = \frac{p_1}{\rho} - \frac{p_2}{\rho} + U_1 - U_2$

$\left(\frac{1}{2} v^2 + \frac{p}{\rho} + U = \text{const.} \right)$ - Bernoulli tr.

lössel Áramlás általános keresztmetszeti csöben

Gaték esetén $\delta f \neq 0$:

$$\delta Q = + \delta E_b + \delta W_b = \delta E_b - \delta W_k$$

↳ Adiabaticus folyamatra $\delta Q = 0$:

$$\frac{1}{2} \Delta m v_2^2 - \frac{1}{2} \Delta m v_1^2 = P_1 A_1 v_1 \Delta t - P_2 A_2 v_2 \Delta t + \Delta m U_1 - \Delta m U_2 + \Delta(-\Delta E_b)$$

$$E_b = m C_v T$$

$$P V = \frac{m}{M} R T \Rightarrow \frac{P}{\rho} = \frac{R}{M} T \quad E_b = m C_v \frac{M}{R} \frac{P}{\rho}$$

$$C_p - C_v = \frac{R}{M} \quad (R-M \text{ egyenlet}) \quad \rightarrow \quad \frac{E_b}{m} = C_v \frac{M}{R} = \frac{C_v}{C_p - C_v} = \frac{1}{\frac{C_p}{C_v} - 1} = \frac{1}{\kappa - 1}$$

$$E_b = m \frac{1}{\kappa - 1} \frac{P}{\rho}$$

⇓

$$\frac{1}{2} v_2^2 - \frac{1}{2} v_1^2 = \frac{P_1}{\rho_1} - \frac{P_2}{\rho_2} + U_1 - U_2 + \frac{1}{\kappa - 1} \frac{P_1}{\rho_1} - \frac{1}{\kappa - 1} \frac{P_2}{\rho_2}$$

$$\left| \frac{1}{2} v^2 + \frac{\kappa}{\kappa - 1} \frac{P}{\rho} + U = \text{állandó} \right|$$

Bernoulli tv. ideális gáson
adiabaticus közlétes esetén

Kiszámítás: lebegő gömb, ^{vezető papír} Pitoté-Prandtl cső, zirkonoksid profil
Áramlás változó keresztmetszeti csöben Magnus-effektus

$$p \cdot A = \text{const}$$

$$\frac{1}{2} v^2 + \frac{\kappa}{\kappa+1} \frac{p}{\rho} + U = \text{const}$$

$$d(p \cdot A) = 0$$

$$v A ds + p A dv + p v dA = 0$$

$$\left| \frac{ds}{s} + \frac{dv}{v} + \frac{dA}{A} = 0 \right|$$

$$U = \text{const}$$

↓

$$v dv + \frac{\kappa}{\kappa-1} \frac{dp}{\rho} - \frac{\kappa}{\kappa-1} \frac{p}{\rho^2} d\rho = 0$$

$$dp = \frac{dp}{ds} ds = c^2 ds$$

↓

$$\frac{2 \frac{1}{2} \frac{1}{2} \frac{1}{2}}{\frac{1}{2}} = \frac{m^2}{s^2}$$

$$v \cdot dv + \frac{\kappa}{\kappa-1} \left(c^2 \frac{ds}{s} - \frac{p}{\rho^2} d\rho \right) = 0$$

$$p \cdot V^\kappa = \text{const}$$

$$\frac{p}{\rho^\kappa} = \text{const} \Rightarrow p = \alpha \cdot \rho^\kappa$$

$$\frac{dp}{d\rho} = \alpha \cdot \kappa \rho^{\kappa-1} = \alpha \cdot \kappa \cdot \frac{\rho^\kappa}{\rho} = \kappa \cdot \frac{p}{\rho}$$

$$v dv + \frac{\kappa}{\kappa-1} \frac{ds}{s} \left(c^2 - \frac{c^2}{\kappa} \right) = 0$$

$$v dv + c^2 \cdot \frac{ds}{s} = 0$$

$$\Rightarrow \frac{ds}{s} = -\frac{v}{c^2} dv$$

→

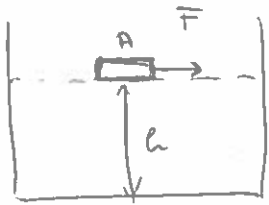
$$\left| -\frac{v}{c^2} dv + \frac{1}{v} dv + \frac{dA}{A} = 0 \right|$$

$$\left| \frac{dv}{v} \left(1 - \frac{v^2}{c^2} \right) + \frac{dA}{A} = 0 \right|$$

$$c^2 = \frac{dF}{dS}$$

Ideális közegben: $\hat{\sigma} = \begin{pmatrix} -P & & \\ & -P & \\ & & -P \end{pmatrix}$

Valódi közegben: $\hat{\sigma} = \begin{pmatrix} -P & & \\ & -P & \\ & & -P \end{pmatrix} + \hat{\sigma}'$



$$F = \eta \frac{A \cdot v}{l} \Rightarrow \tau = \eta \frac{dv_x}{dy}$$

Newton-féle viszkozitás

$$\underline{F}(x, y, t)$$

$$\hat{\sigma}(\hat{\epsilon}, \dot{\hat{\epsilon}}, t)$$

Forrás: $\hat{\sigma}'(\dot{\hat{\epsilon}})$

$$\dot{\hat{\epsilon}}_{ij} = \frac{1}{2} \left(\frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} \right)$$

$$\sigma_{ij} = 2\mu \epsilon_{ij} + \lambda \delta_{ij} \epsilon_{ee}$$

Hasonlóan (isz. horgás): $\sigma'_{ij} = 2\eta \dot{\epsilon}'_{ij} + \eta' \delta_{ij} \dot{\epsilon}'_{ee}$

$$\frac{\partial}{\partial x_i} \sigma'_{ij} = \eta \frac{\partial}{\partial x_i} \left(\frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} \right) + \eta' \frac{\partial}{\partial x_j} \frac{\partial v_e}{\partial x_i} =$$

$$= \eta \frac{\partial^2}{\partial x_i^2} v_j + (\eta + \eta') \frac{\partial}{\partial x_j} \frac{\partial}{\partial x_i} v_i$$

$$\text{div } \hat{\sigma}' = \eta \Delta \underline{v} + (\eta + \eta') \text{grad}(\text{div } \underline{v}) \leftarrow \text{Összenghetetlen fejedlőre a ? null}$$

Eddig: $\nabla \cdot \underline{S} = \text{div } \underline{G} + \underline{f}$

↳ Hogy néz ez ki a sebességkibén? $\underline{v}(\underline{r}, t)$

$\underline{v}(\underline{r}(t), t)$

↳ részecske koordinátája

részecske mozgása:

$$\frac{d}{dt} v_i(\underline{r}(t), t) = \frac{\partial v_i}{\partial t} + \frac{\partial v_i}{\partial r_j} \cdot v_j$$

$$\frac{d}{dt} \underline{v}(\underline{r}(t), t) = \frac{\partial \underline{v}}{\partial t} + (\underline{v} \cdot \nabla) \underline{v}$$

↓

$$\left\{ \begin{array}{l} \rho \frac{\partial \underline{v}}{\partial t} + \rho (\underline{v} \cdot \nabla) \underline{v} = - \text{grad } p + \underline{\eta \Delta \underline{v}} + (\eta + \eta') \text{grad}(\text{div } \underline{v}) \\ \frac{\partial \rho}{\partial t} + \text{div}(\rho \underline{v}) = 0 \end{array} \right. \quad \text{Navier-Stokes}$$

~~$p(\underline{r})$~~

$p(\underline{r}) \leftarrow$ \neq gáz viselkedése

(+ hőmérséklet latin' gyanút)

Két == by arány: v_0 - karakterisztikus sebesség
 l - karakterisztikus méret

$$\rho \cdot \frac{v_0^2}{l} / \eta \frac{v_0}{l^2} = \frac{\rho}{\eta} \cdot v_0 \cdot l =: R \quad \text{dimenziótlós szám}$$

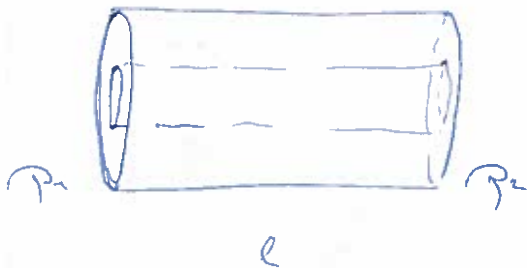
↳ Reynold - szám



Ho a Reynold-szám kicsi, akkor a nemlinearitás nem számít.

↳ a N-S egyenlet statisztikus megoldása.

Árcsőlés csövek



$$\eta \Delta v + (\eta + \eta') \operatorname{grad}(\operatorname{div} v)$$

$$\oint \hat{\sigma} dA = 0$$

$$\tau = \eta \frac{dv}{dr}$$

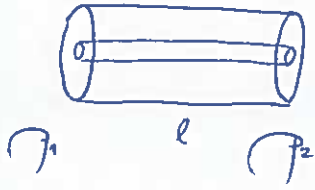
$$2\pi r l \cdot \eta \frac{dv}{dr} - (P_2 - P_1) r^2 \pi = 0$$

$$2l\eta \frac{dv}{dr} = + (P_2 - P_1) \cdot r$$

$$\frac{dv}{dr} = - \frac{P_1 - P_2}{2l\eta} \cdot r \Rightarrow v(r) = - \frac{P_1 - P_2}{4l\eta} \cdot r^2 + C$$

↳ A határfeltétel nem adott (rézcső, vascső)

$$\hookrightarrow v(R) = 0$$



$$\oint \hat{G} dA = 0$$

$$v(r) = - \frac{p_1 - p_2}{4\eta l} r^2 + C \quad v(R) = 0$$

↓

$$v(r) = \frac{p_1 - p_2}{4\eta l} (R^2 - r^2)$$

Mennyi mennyit árt időegység alatt?

$$\dot{\phi} = \int_{\sigma_n} \rho v(r) dA$$

$$= \int_0^R \frac{p_1 - p_2}{4\eta l} \cdot (R^2 - r^2) 2r\pi \cdot dr = \frac{p_1 - p_2}{2\eta l} \pi \int_0^R (R^2 - r^2) r \cdot dr =$$

$$= \frac{p_1 - p_2}{2\eta l} \pi \left[\frac{R^3}{3} - \frac{r^3}{3} \right] = \frac{p_1 - p_2}{8\eta l} \pi R^3 \quad H-P \text{ tv.}$$

Turbulens áramlás

↳ vides

$$\frac{\partial \rho}{\partial t} + \text{div}(\rho v) = 0$$

$$\rho \left[\frac{\partial v}{\partial t} + (v \cdot \nabla) v \right] = -\text{grad} p + \text{div} \hat{\sigma}' + f$$

$\rho(\rho)$

↳ Van egy megoldás: $\rho = \rho_0 = \text{állandó} \Rightarrow \rho(\rho) = \text{állandó}$

$$v = 0$$

p és p' is:

$$p = p_0 + \delta p$$

\underline{v} (pisc) (és a deriváltai is)

$$\frac{\partial \delta p}{\partial t} + p_0 \cdot \text{div} \underline{v} = 0$$

$$p_0 \frac{\partial \underline{v}}{\partial t} = -c^2 \text{grad} \delta p$$

$$p_0 \left[\frac{\partial \underline{v}}{\partial t} + 0 \right] = - \left. \frac{dp}{ds} \right|_{p_0} \text{grad} \delta p \quad c^2 := \left. \frac{dp}{ds} \right|_{p_0}$$

$$\Downarrow$$

$$\left. \begin{aligned} \frac{\partial^2 \delta p}{\partial t^2} + p_0 \cdot \text{div} \frac{\partial \underline{v}}{\partial t} &= 0 \\ p_0 \text{div} \frac{\partial \underline{v}}{\partial t} &= -c^2 \Delta \delta p \end{aligned} \right\}$$

$$\frac{\partial^2 \delta p}{\partial t^2} - c^2 \Delta \delta p = 0$$

é hullímegegyenlet

$$\frac{\partial^2 \delta p}{\partial t^2} - c^2 \Delta \delta p = 0$$

1. $\left. \frac{dp}{ds} \right|_{p_0}$

$$\frac{\partial}{\partial t} \text{grad} \delta p + p_0 \Delta \underline{v} = 0$$

$$p_0 \cdot \frac{\partial^2 \underline{v}}{\partial t^2} = -c^2 \cdot \frac{\partial}{\partial t} \text{grad} \delta p$$

$$p_0 \cdot \frac{\partial^2 \underline{v}}{\partial t^2} = +c^2 p_0 \overset{\text{grad div}}{\Delta} \underline{v} \Rightarrow$$

$$\frac{\partial^2 \underline{v}}{\partial t^2} - c^2 \overset{\text{grad div}}{\Delta} \underline{v} = 0$$

\Downarrow

$$\Rightarrow p_0 \frac{\partial}{\partial t} \text{rot} \underline{v} = -c^2 \text{rot grad} \delta p = 0$$

\Downarrow

$$\text{rot} \underline{v} = 0 \quad (\text{ke kezdletheen is})$$

$$\left. \begin{aligned} \frac{\partial^2}{\partial t^2} (\text{div} \underline{v}) - c^2 \Delta (\text{div} \underline{v}) &= 0 \\ \text{rot} \underline{v} &= 0 \end{aligned} \right\}$$

Mi lehet a megoldás?

$$\delta s = \delta s_0 \cdot e^{i(\omega t + \underline{k} \cdot \underline{r})} \leftarrow \text{síkhullám}$$

$$\frac{\partial^2 \delta s}{\partial t^2} = -\omega^2 \delta s \quad ; \quad \Delta \delta s = -(\underline{k}_x^2 + \underline{k}_y^2 + \underline{k}_z^2) \delta s = -|\underline{k}|^2 \delta s \Rightarrow -\omega^2 + c^2 |\underline{k}|^2 = 0$$

$$\boxed{\omega = c |\underline{k}|}$$

\underline{k} : hullámhossz vektor

$$\lambda = \frac{2\pi}{|\underline{k}|} \quad ; \quad \text{hullámhossz}$$

$$\underline{v} = \underline{v}_0 \cdot e^{i(\omega t + \underline{k} \cdot \underline{r})}$$

$$\text{rot } \underline{v} = (\underline{k} \times \underline{v}_0) e^{i(\omega t + \underline{k} \cdot \underline{r})} = 0 \Rightarrow \underline{v}_0 \parallel \underline{k} \quad (\text{különben rot } \underline{v} \neq 0)$$

\hookrightarrow longitudinális hullám.

Hokirilet: gázcső rezgése hanggal.

$$\left. \frac{dp}{ds} \right|_{s_0} = ?$$

$$pV^k = \text{all} \Rightarrow \frac{p}{s^k} = \text{all} \Rightarrow p = \text{all } s^k \Rightarrow \frac{dp}{ds} = k \cdot \text{all } s^{k-1} =$$

\uparrow
Adiabátikus

$$= \frac{k}{s} p = k \frac{p}{s} = \boxed{k \frac{R}{M} T}$$

$$\Leftrightarrow c^2 = k \frac{R}{M} T$$

Isoterm:

$$p = s \frac{R}{M} T \Rightarrow \boxed{\frac{dp}{ds} = \frac{R}{M} T}$$

Nagy fokú: $c^2 = k \frac{R}{M} T$

Kis fokú: $c^2 = \frac{R}{M} T$

A hengerben a hővezetés nem figyelhető meg (disperzió (itt pici))

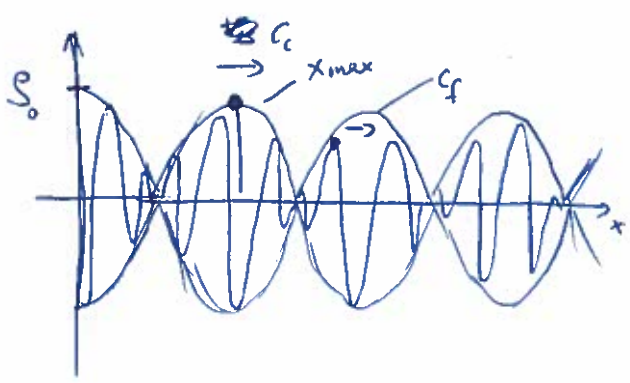
$c^2 = \frac{dP}{dS}$ - függ az állapotváltozástól

↳ Adiabaticus: $\frac{P}{\rho^{1/\kappa}} = \text{állandó}$
 ↳ izoterm: $\frac{P}{\rho} = \text{állandó}$ } extrin esetek $\omega \rightarrow \infty$
 $\omega \rightarrow 0$

↙
 $c(\omega)$ - diszperzió

Allalósiabbon: $\omega(k)$ $\frac{\omega}{k} = c$

$S = S_0 \sin(\omega_1 t + k_1 x) + S_0 \sin(\omega_2 t + k_2 x) =$
 $= 2S_0 \cos\left(\frac{\omega_1 - \omega_2}{2} t + \frac{k_1 - k_2}{2} x\right) \sin\left(\frac{\omega_1 + \omega_2}{2} t + \frac{k_1 + k_2}{2} x\right)$
 // $\sin(\alpha + \beta) = 2 \cdot \cos \frac{\alpha - \beta}{2} \sin \frac{\alpha + \beta}{2}$



$x_{\text{max}} \approx -c_c \cdot t$
 $\left[c_c = \frac{\omega_1 - \omega_2}{k_1 - k_2} \approx \frac{d\omega}{dk} \right]$ csopant sebesség

$\left[c_f = \frac{\omega_1 + \omega_2}{k_1 + k_2} \approx \frac{\omega}{k} \right]$ fázis sebesség

Horglan = optika (horg longitudinális, korg transverzális)

Sírtöréskörvény:

$\underline{S}_{\perp} = \text{div } \underline{\hat{G}} + \underline{f}$ $\underline{\hat{G}}(\underline{\hat{z}}) = 2\mu \underline{\hat{z}} + \lambda \underline{\hat{z}} \cdot \text{Sp}(\underline{\hat{z}})$

$$\varepsilon_{ij} = \frac{1}{2} (\partial_j u_i + \partial_i u_j)$$

↓

$$\sigma_{ij} = \mu (\partial_j u_i + \partial_i u_j) + \lambda \delta_{ij} \partial_k u_k$$

$$\begin{aligned} (\text{div } \hat{\sigma})_j &= \partial_i \sigma_{ij} = \mu \partial_i \partial_j u_i + \mu \partial_i^2 u_j + \lambda \partial_j \partial_k u_k = \\ &= (\mu + \lambda) \partial_j \partial_i u_i + \mu \partial_i^2 u_j \end{aligned}$$

↓

$$\rho \underline{\ddot{u}} = (\lambda + \mu) \text{grad}(\text{div } \underline{u}) + \mu \Delta \underline{u} + \underline{f} \quad \leftarrow \text{keresj meg ezeket}$$

↳ Nullát ezeket $\underline{f} \approx 0$, mert a rugalmas állapothoz képest reziliens

div ↘

$$\rho \partial_t^2 (\text{div } \underline{u}) = (\lambda + \mu) \Delta (\text{div } \underline{u}) + \mu \Delta (\text{div } \underline{u}) = (\lambda + 2\mu) \Delta (\text{div } \underline{u})$$

$$\underline{\partial_t^2 (\text{div } \underline{u})} = \underline{c_L^2 \Delta (\text{div } \underline{u})} \quad c_L^2 = \frac{\lambda + 2\mu}{\rho}$$

↳ relatív térfogatváltozás

rot ↙

$$\rho \partial_t^2 (\text{rot } \underline{u}) = \mu \Delta (\text{rot } \underline{u})$$

$$\underline{\partial_t^2 (\text{rot } \underline{u})} = \underline{c_T^2 \Delta (\text{rot } \underline{u})} \quad c_T^2 = \frac{\mu}{\rho}$$

$$\underline{u} = \underline{u}_L + \underline{u}_T \quad \text{felbontás: } \text{rot } \underline{u}_L = 0 \quad ; \quad \text{div } \underline{u}_T = 0$$

$$\text{rot} \left(\underline{u}_0 e^{i(\omega t + \underline{k}r)} \right) = \underline{0} \quad i(\underline{k} \times \underline{u}_0) e^{i(\omega t + \underline{k}r)} = 0$$

$\hookrightarrow \underline{k} \parallel \underline{u}_0 \rightarrow$ longitudinális

$$\text{div} \left(\underline{u}_0 e^{i(\omega t + \underline{k}r)} \right) = i \underline{k} \cdot \underline{u}_0 e^{i(\omega t + \underline{k}r)} = 0$$

$\hookrightarrow \underline{u}_0 \perp \underline{k} \rightarrow$ transverzális

\hookrightarrow Hang terjedési sebességét λ és μ meghatározhatjuk.

Hogyan kapcsolódik a sírhullámok rezgése a hanghullámokhoz?

$$\underline{S} \cdot \underline{u} = \text{div } \hat{G}$$

Minden közegben
érvényes

gáz / szilárd

A sírhullámok minden egyes felületi komponensét külön-külön megnézhetjük.

\hookrightarrow A hullámok összetételének

\downarrow

A hang nyomóhullám

(Fresnel-formulákhoz hasonló
képleteket lehet kapni)

1D-ben:

$$\rho \frac{\partial^2 u(x,t)}{\partial t^2} = \frac{\partial}{\partial x} G(x,t)$$

$$G(x,t) = E \frac{\partial u}{\partial x}$$

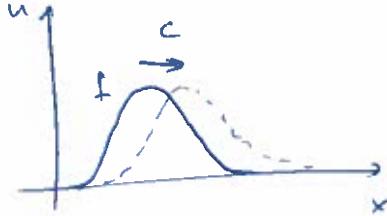
$$\rho \frac{\partial^2 u}{\partial t^2} = E \frac{\partial^2 u}{\partial x^2}$$

$$c^2 = \frac{E}{\rho}$$

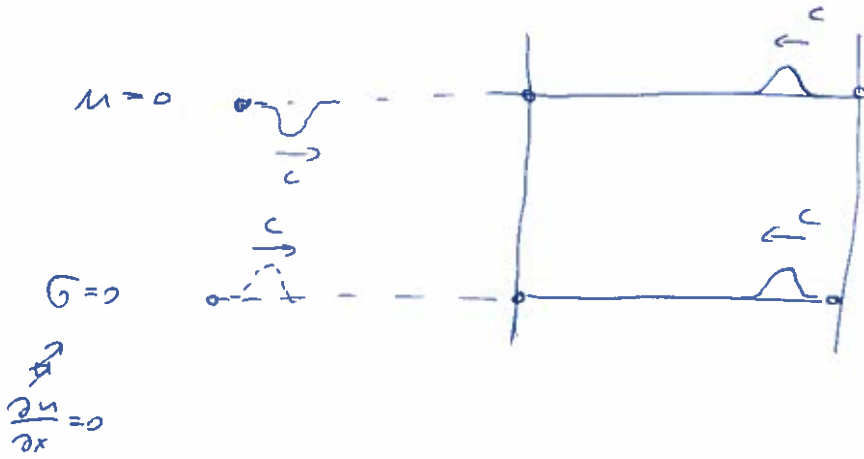
$$\left| \frac{\partial^2 u}{\partial t^2} = c^2 \frac{\partial^2 u}{\partial x^2} \right|$$

Hullámegyenlet

$u = f(x \pm ct)$ - megoldás

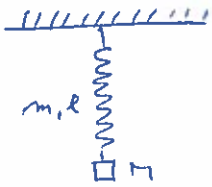


Mi van a helyénél?



"nőzést vég"

"hábad vég"



$$S \frac{\partial^2 u}{\partial t^2} = E \frac{\partial^2 u}{\partial x^2} + \underbrace{f}_{Sg}$$

leghalibb pont: $M \frac{d^2 u(l,t)}{dt^2} = Mg - E \frac{\partial u}{\partial x}(l,t) - A$

legfeljebb $u(0,t) = 0$

$$u(x,t) = b \cdot \sin(\omega t + \varphi) \cdot \sin(kx)$$

$$\omega^2 = \frac{E}{S} k^2$$

$$-S \omega^2 u = -E k^2 u$$

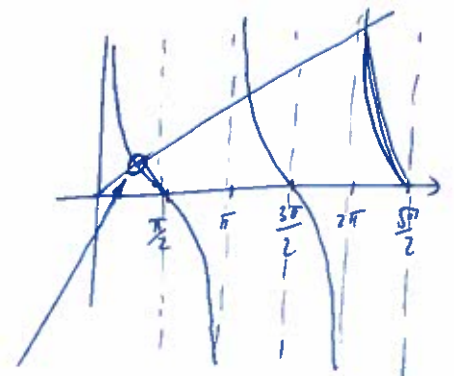
$$M \omega^2 \sin(kl) = A E k \cos(kl) \quad (\text{határofeltétel})$$

↘

$$M \omega^2 \frac{E}{S} k \sin(kl) = A E k \cos(kl)$$

$$M \frac{1}{S l} (kl) = A \frac{\cos(kl)}{\sin(kl)} = z$$

$$\frac{M}{m} (kl) = z \quad \xrightarrow{\text{grafikonon}}$$



$kl = \text{const}$ a legalszorosabb frekvenciájú megoldás marad meg, a többi kihel.

$m \ll M$ eset:

$$c_f(x) = \frac{\cos(x)}{\sin(x)} = \frac{1 - \frac{x^2}{2} + \dots}{x - \frac{x^3}{6} + \dots} \approx \frac{1}{x} \frac{1 - \frac{x^2}{2}}{1 - \frac{x^2}{6}} \approx \frac{1}{x} \left(1 - \frac{x^2}{2}\right) \left(1 + \frac{x^2}{6}\right) \approx$$

$$\approx \frac{1}{x} \left(1 - \frac{x^2}{3}\right) = \frac{1}{x} - \frac{x}{3}$$

↙

$$\frac{M}{m}(kl) = \frac{1}{kl} - \frac{bl}{3}$$

$$\left(\frac{M}{m} + \frac{1}{3}\right)(kl) = \frac{1}{kl} \Rightarrow kl^2 = \frac{3m}{3M+m} = \frac{m}{M + \frac{m}{3}}$$

$$\Rightarrow \omega^2 = \frac{E}{S} \frac{1}{l^2} \frac{m}{M + \frac{m}{3}} = \frac{E}{l} \cdot \frac{m}{Sl} \frac{1}{M + \frac{m}{3}}$$

$$\boxed{\omega^2 = \frac{E \cdot A}{l} \frac{1}{M + \frac{m}{3}} = \frac{D}{M + \frac{m}{3}}}$$

leeső ~~nyel~~

$$S \frac{\partial^2 u}{\partial t^2} = E \frac{\partial^2 u}{\partial x^2} + Sg$$

$$u_\infty(x) = \frac{Sg}{E} \left(lx - \frac{x^2}{2} \right)$$

$$\frac{\partial u}{\partial x}(0) = 0 \quad \frac{\partial u}{\partial x}(l) = 0$$

$$u(x,t) = u_\infty(x) + u'(x,t)$$

$$u'(x,0) = 0$$

$$\boxed{S \frac{\partial^2 u'}{\partial t^2} = E \frac{\partial^2 u'}{\partial x^2}}$$

$$\frac{\partial u}{\partial x}(l) = \frac{\partial u_\infty}{\partial x}(l) + \frac{\partial u'}{\partial x}(l) \stackrel{!}{=} 0$$

$$\frac{\partial u}{\partial x}(0) = \frac{\partial u_\infty}{\partial x}(0) + \frac{\partial u'}{\partial x}(0) \stackrel{!}{=} 0$$

↑
Sgl

$$\boxed{\frac{\partial u'}{\partial x}(l) = 0} \quad \boxed{u'(x,0) = 0}$$

$$\frac{\partial u'}{\partial x}(0) = -\frac{Sg}{E}l$$

$$0 < x < l$$

$$f(x - ct)$$

$$c^2 = \frac{E}{\rho}$$



$$f_{gd} = + \frac{SgR}{E}$$

$$P(1) = N P(\tau) \Delta \tau \cdot (1 - P(\tau) \Delta \tau)^{N-1}$$

~~$$P(0) = P(\tau) 2 \Delta \tau$$~~

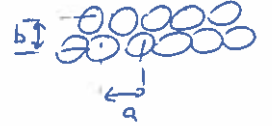
$$P(2) = \frac{N \cdot (N-1)}{2} P(\tau) (2\Delta\tau)^2 \cdot (1 - P(\tau) 2\Delta\tau)^{N-2} \cdot \frac{3}{4}$$



Elméleti feszítési törvény

$$\sigma = \frac{a}{b} \cdot \frac{1}{\pi} \left| \sin\left(\frac{\pi x}{a}\right) \right|$$

$$\sigma_{\max} \approx \frac{a}{\pi} \approx 100 \text{ MPa}$$



$$K = \frac{a}{b} \cdot \frac{1}{\pi}$$

Diszlokációk

↳ erővel és rugalmas térben